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# CALPHAD: Computer Coupling of Phase Diagrams and Thermochemistry

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## Solution-based thermodynamic modeling of the Ni–Ta and Ni–Mo–Ta systems using first-principle calculations

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### ABSTRACT

Solution-based thermodynamic descriptions of the Ni–Ta and Ni–Mo–Ta systems are developed with supporting first-principles calculations and reported experimental data for parameter evaluation. For the Ni–Ta system, the liquid, bcc and fcc phases are described with a random solution model,  $\text{DO}_{22}\text{-Ni}_3\text{Ta}$  is treated as a stoichiometric compound, and the remaining compounds are modeled as solid solutions on multiple sublattices. The resulting model for the Ni–Ta system is integrated with reported treatments of the Ni–Mo and Mo–Ta systems, and a thermodynamic model for the ternary Ni–Mo–Ta system is developed. The zero-Kelvin enthalpies of formation for the intermetallic compounds in the Ni–Mo–Ta system and the enthalpies of mixing for the bcc and fcc special quasirandom structures (SQS) in the binary Ni–Ta system are computed using the Vienna Ab-initio Simulation Package (VASP). Phase equilibria modeling results for the ternary Ni–Mo–Ta system are summarily presented in the form of isothermal sections and liquidus projections, with appropriate comparisons with available experimental data.

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### 1. Introduction

High temperature performance is a critical issue for power generation and transportation applications of Ni-based superalloys, and considerable effort has been devoted to the development of the thermodynamic models required to describe phase stability at elevated temperatures in these materials [1–9]. Specifically, it is necessary to understand the thermodynamic effects of alloying elements, such as Ta and Mo, which play an important role in strategies for increasing the high temperature stability of  $\gamma/\gamma'$  microstructures. To this end, we focus here on the development of reliable thermodynamic models for the Ni–Ta and Ni–Ta–Mo alloy systems.

Thermodynamic modeling of the Ni–Ta binary system was reported by Kaufman [4] and by Ansara and Selleby [5]. In each of these approaches, a total of eight phases were considered. The liquid, fcc, and bcc phases were treated as single-sublattice solutions, while the  $\text{C16-NiTa}_2$ ,  $\mu\text{-NiTa}$ ,  $\text{C11}_b\text{-Ni}_2\text{Ta}$ ,  $\kappa\text{-Ni}_3\text{Ta}$ , and  $\zeta\text{-Ni}_8\text{Ta}$  phases were treated as stoichiometric compounds. Subsequently, in order to model the solubility ranges exhibited by

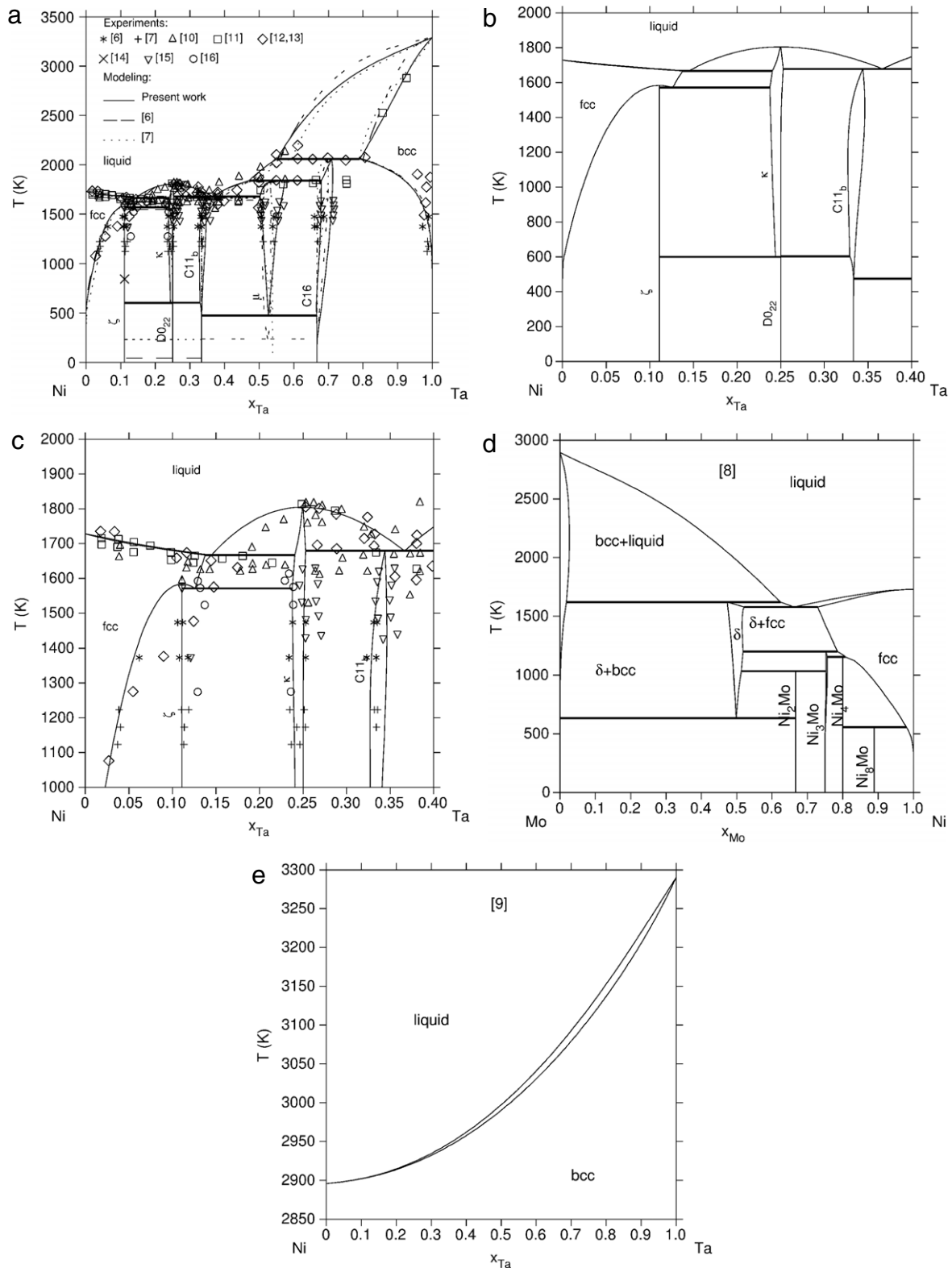
certain intermetallic phases, Cui and Jin (CJ) [6] described the  $\kappa\text{-Ni}_3\text{Ta}$  and  $\text{C16-NiTa}_2$  phases with two-sublattices and the  $\mu\text{-NiTa}$  phase with four-sublattices. Pan and Jin (PJ) [7] further refined the model by adding a two-sublattice treatment for the  $\text{C11}_b\text{-Ni}_2\text{Ta}$  phase and reassessing the system, reducing the total number of thermodynamic parameters. The Ni–Ta binary phase diagrams associated with these modeling efforts are shown in Fig. 1, along with relevant experimental data [6,7,10–16]. In addition, Figs. 2 and 3 show that the calculated enthalpy of formation for the compounds at 298 K and enthalpy of mixing for liquid at 1873 K using both the CJ [6] and PJ [7] models differ substantially from reported measurements.

For the Ni–Mo–Ta ternary system, CJ also reported [9] an assessment based on the binary model parameters for the Ni–Mo [9], Mo–Ta [9], and Ni–Ta [6] systems. In their treatment, they model the  $\text{DO}_a\text{-Ni}_3\text{Mo}$  and  $\kappa\text{-Ni}_3\text{Ta}$  phases as a single phase. While this approach is reasonable since the two structures differ only in layer packing sequence, the phases are clearly distinct, and we treat them separately here. In addition, the present model incorporates a more recent description of the Ni–Mo system [8] as shown in Fig. 1(d) and a new assessment of the Ni–Ta binary. In subsequent sections of this paper, we will discuss these differences further and present the refined model, which offers better agreement with the experiment.

In the present work, the thermodynamic properties of the Ni–Ta and Ni–Mo–Ta systems and the associated phase equilibria are

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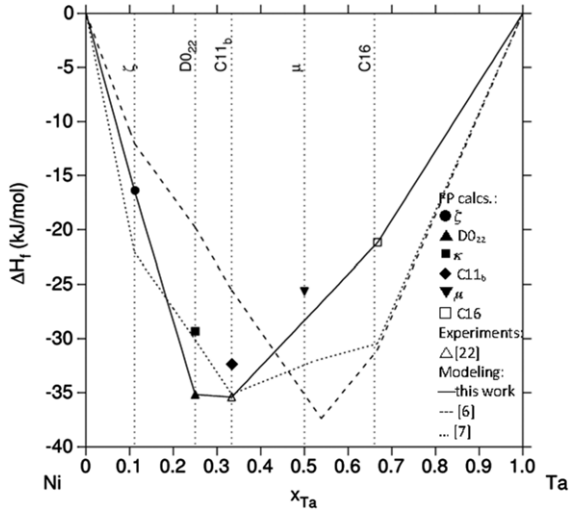


**Fig. 1.** The Ni-Ta phase diagram computed from the current model (a) shown over the full range of composition, compared with previous models and reported experimental data and shown over the Ni-rich portion of the binary range, without (b) and with (c) relevant experimental data. The Ni-Mo and Mo-Ta phase diagram plotted in (d) and (e) respectively.

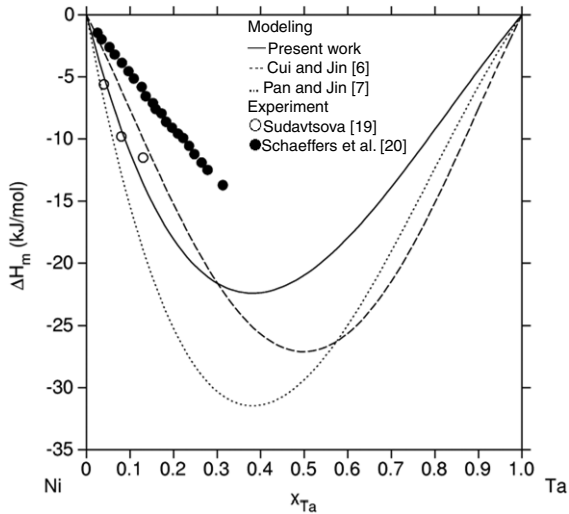
described by incorporating the first-principles calculations into a general CALPHAD [17,18] approach. The evaluation starts with the binary Ni-Ta system, for which the thermodynamic parameters are evaluated with the first-principles calculated enthalpies of formation and all available experimental data [6,7,10–16,19–22]. Special

quasirandom structures (SQS) [23,24] are used to calculate the enthalpies of mixing for the bcc and fcc phases from first-principles, and the results are incorporated into the comprehensive model.

For the ternary Ni-Mo-Ta system, a distinguishing feature of our approach, in comparison with that reported in Ref [9], is



**Fig. 2.** The enthalpy of formation of the Ni–Ta system, as computed using the present model, shown with first-principles calculations and reported experimental data.



**Fig. 3.** The enthalpy of mixing in liquid at 1873 K, as computed using the present model. Reported experimental data and prior modeling are also shown.

that we allow for Mo–Ta substitution. For example, the stable  $\text{D0}_a\text{-Ni}_3\text{Mo}$  and metastable  $\text{D0}_a\text{-Ni}_3\text{Ta}$  phases ( $\text{Cu}_3\text{Ti}$  structure [25,26]) are treated as a single solution phase denoted by  $\text{D0}_a\text{-Ni}_3(\text{Mo}, \text{Ta})$ . Similarly, the metastable  $\kappa\text{-Ni}_3\text{Mo}$  and stable  $\kappa\text{-Ni}_3\text{Ta}$  phases ( $\text{Pt}_3\text{Ta}$  structure [25,26]) are described as  $\kappa\text{-Ni}_3(\text{Mo}, \text{Ta})$ , and the stable  $\text{Ni}_8\text{Ta}$  and  $\text{Ni}_8\text{Mo}$  phases ( $\text{Ni}_8\text{Nb}$  structure [14]) are described as  $\zeta\text{-Ni}_8(\text{Mo}, \text{Ta})$ . The ternary parameters for the individual phases are evaluated using all available experimental information [9,27–29], and the resulting model for phase equilibria in this ternary system are presented in the forms of liquidus projections and isothermal sections of the phase diagram.

## 2. Thermodynamic models

The phases considered in the present model are listed in Table 1, indicating the symbol to be used in this paper and the prototype structure. The thermodynamic properties of pure Ni, Mo, and Ta in the various relevant structures are computed using the parameters from the SGTE database [30], as listed in Table 2. In addition to the compounds in the Ni–Mo system described in Ref. [8], the fcc, bcc and liquid phases are modeled as simple ternary

**Table 1**  
A listing of phases modeled in the current treatment.

Formula unit	Sym.	Lattice	Struk. Des.	Prototype	Ref.
Phases extending from the pure component states:					
Ni, Ta, Mo	–	–	–	Liquid	–
Ni	–	cub	A1	fcc	–
Ta	–	cub	A2	bcc	–
Mo	–	cub	A2	bcc	–
Phases extending from the Ni–Ta binary system:					
$\text{NiTa}_2$	–	tet	C16	$\text{Al}_2\text{Cu}$	[33]
$\text{NiTa}$	$\mu$	trig	$\text{D8}_5$	$\text{Fe}_7\text{W}_6$	[33]
$\text{Ni}_2\text{Ta}$	–	tet	C11 <sub>b</sub>	$\text{MoSi}_2$	[25,26]
$\text{Ni}_3\text{Ta}$	$\kappa$	mono	–	$\text{Pt}_3\text{Ta}$	[25,26]
$\text{Ni}_8\text{Ta}$	$\zeta$	tet	–	$\text{Al}_3\text{Ti}$	[25,26]
Phases extending from the Ni–Mo binary system:					
$\text{NiMo}$	$\delta$	orth	–	$\text{NiMo}$	[25]
$\text{Ni}_2\text{Mo}$	–	tet	–	$\text{Pt}_2\text{Mo}$	[34]
$\text{Ni}_3\text{Mo}$	–	tet	$\text{D0}_a$	$\text{Cu}_3\text{Ti}$	[25]
$\text{Ni}_4\text{Mo}$	–	tet	$\text{D1}_a$	$\text{Ni}_4\text{Mo}$	[25]
$\text{Ni}_8\text{Mo}$	$\zeta$	tet	–	$\text{Ni}_8\text{Nb}$	[14]

substitutional solutions, the C16– $\text{NiTa}_2$ ,  $\mu\text{-NiTa}$ , C11<sub>b</sub>– $\text{Ni}_2\text{Ta}$ ,  $\kappa\text{-Ni}_3(\text{Mo}, \text{Ta})$ ,  $\text{D0}_a\text{-Ni}_3(\text{Mo}, \text{Ta})$  and  $\zeta\text{-Ni}_8(\text{Mo}, \text{Ta})$  intermetallic phases are described with a sublattice formalism [31], while the  $\text{D0}_{22}\text{-Ni}_3\text{Ta}$  phase is treated as stoichiometric compound in the ternary Ni–Mo–Ta system. The thermodynamic models are defined in Table 3, where the total Gibbs free energy for any phase,  $\Phi$ , is generally given by the sum of three contributions,

$$G_m^\Phi = {}^{\text{ref}}G_m^\Phi + {}^{\text{id}}G_m^\Phi + {}^{\text{xs}}G_m^\Phi, \quad (1)$$

where the subscript  $m$  denote that all terms are molar quantities of formula unit. The first term in Eq. (1) is given by the sum of occupancy-weighted sublattice end-member contributions. The second and third terms are the ideal and excess parts of the Gibbs free energy of mixing, respectively. In Table 3, a Redlich–Kister polynomial [32] is used to describe the composition and temperature dependence of the excess Gibbs free energy associated with mixing. The specific treatment of each phase is discussed briefly here.

The liquid, fcc and bcc phases are described with a single lattice, using the model given in Table 3, where  ${}^0G_i^\Phi$  is the molar Gibbs free energy of the pure element  $i$  with the structure  $\Phi$  ( $\Phi = \text{liquid}, \text{fcc}$  or  $\text{bcc}$ ), as listed in Table 2, and  $x_i$  is the mole fraction of the indicated component  $i$ .  ${}^jL_{i,k}^\Phi$  is the binary interaction parameter, and  $L_{\text{Mo,Ni,Ta}}^\Phi$  is a composition dependent ternary interaction parameter, expressed as  $L_{\text{Mo,Ni,Ta}}^\Phi = x_{\text{Mo}}{}^0L_{\text{Mo,Ni,Ta}}^\Phi + x_{\text{Ni}}{}^1L_{\text{Mo,Ni,Ta}}^\Phi + x_{\text{Ta}}{}^2L_{\text{Mo,Ni,Ta}}^\Phi$ , where the parameters  ${}^0L_{\text{Mo,Ni,Ta}}^\Phi$ ,  ${}^1L_{\text{Mo,Ni,Ta}}^\Phi$  and  ${}^2L_{\text{Mo,Ni,Ta}}^\Phi$  may be temperature dependent and are evaluated with experimental data.

The  $\mu\text{-NiTa}$  phase has been reported [33] to have a rhombohedral structure ( $\text{Fe}_7\text{W}_6$  prototype) with a primitive unit cell of 13 atoms, distributed in five sublattices as  $(\text{Ni}, \text{Ta})_1^1(\text{Ta})_2^{15}(\text{Ta})_2^{16}(\text{Ni}, \text{Ta})_2^{14}(\text{Ni}, \text{Ta})_6^{12}$ . (The subscript is the number of sites in that sublattice, and the superscript is the coordination number.) The analysis by Andersson et al. [35], later showed that fcc and bcc elements prefer sublattices with a coordination numbers of 12 while bcc elements prefer sublattices with coordination numbers of 14 and 15. This led to the use of a four-sublattice model by Ansara et al. [36] and was supported by the investigation of Joubert and Dupin [37], where the atom distribution was confirmed to be  $(\text{Ni}, \text{Ta})_1(\text{Ta})_4(\text{Ni}, \text{Ta})_2(\text{Ni}, \text{Ta})_6$ , which we adopt here. The corresponding Gibbs free energy terms are given in Table 3, where  $y^I$ ,  $y^{\text{III}}$ , and  $y^{\text{IV}}$  are the site occupancy fractions in the first, third and fourth sublattices, respectively.  ${}^kL^\mu$  is the  $k$ th interaction parameter, expressed as  ${}^ka^\mu + {}^kb^\mu T$ .  ${}^0G_{i_1\text{Ta}_4j_2k_6}^\mu$  represents the Gibbs free energy of the end-members  $(i)_1(\text{Ta})_4(j)_2(k)_6$  with the Gibbs free energy of formation,  $\Delta_{i_1\text{Ta}_4j_2k_6}^\mu$ , being expressed as  $a_{i_1\text{Ta}_4j_2k_6}^\mu + b_{i_1\text{Ta}_4j_2k_6}^\mu T$ . Considering the composition range of  $\mu\text{-NiTa}$  phase being around 0.5, the

**Table 2**  
The thermodynamic parameters for pure elements [30].

Mo phases							
	${}^0G_{\text{Mo}}^{\text{liq}}$		${}^0G_{\text{Mo}}^{\text{bcc}}$		${}^0G_{\text{Mo}}^{\text{fcc}}$		
$T_{\text{min}}$	298	2896	298	2896	298	2896	298
$T_{\text{max}}$	2896	5000	2896	3200	2896	3200	5000
${}^0G^{\text{ref}}$	${}^0G_{\text{Mo}}^{\text{bcc}}$		-		-		${}^0G_{\text{Mo}}^{\text{fcc}}$
$a_0$	41831.347	3538.963	-7746.302	-30556.41	-30556.41	-30556.41	15200
$a_1$	-14.694912	271.6697	131.9197	283.559746	283.559746	283.559746	0.63
$a_2$	-	-42.63829	-23.56414	-42.63829	-42.63829	-42.63829	-
$a_3$	-	-	-0.003443396	-	-	-	-
$a_4$	-	-	$5.66283 \times 10^{-7}$	-	-	-	-
$a_5$	-	-	$-1.30927 \times 10^{-10}$	-	-	-	-
$a_6$	-	-	65812.39	-	-	-	-
$a_7$	-	-	-	-4.849315 $\times 10^{33}$	-4.849315 $\times 10^{33}$	-4.849315 $\times 10^{33}$	-
$a_8$	$4.24519 \times 10^{-22}$	-	-	-	-	-	-
Ni phases							
	${}^0G_{\text{Ni}}^{\text{liq}}$		${}^0G_{\text{Ni}}^{\text{bcc}}$		${}^0G_{\text{Ni}}^{\text{fcc}}$		
$T_{\text{min}}$	298	1728	298	298	298	298	1728
$T_{\text{max}}$	1728	6000	6000	6000	1728	1728	6000
${}^0G^{\text{ref}}$	${}^0G_{\text{Ni}}^{\text{fcc}}$		-		-		-
$a_0$	16414.686	-9549.775	8715.084	-5179.159	-5179.159	-5179.159	-27840.655
$a_1$	-9.397	268.598	-3.556	117.854	117.854	117.854	279.135
$a_2$	-	-43.1	-	-22.096	-22.096	-22.096	-43.1
$a_3$	-	-	-	-0.0048407	-0.0048407	-0.0048407	-
$a_4$	-	-	-	-	-	-	-
$a_5$	-	-	-	-	-	-	-
$a_6$	-	-	-	-	-	-	-
$a_7$	-	-	-	-	-	-	$1.12754 \times 10^{31}$
$a_8$	$-3.82318 \times 10^{-21}$	-	-	-	-	-	-
$T_c$	-	-	575	633	633	633	-
$\beta$	-	-	0.85	0.52	0.52	0.52	-
Ta phases							
	${}^0G_{\text{Ta}}^{\text{liq}}$		${}^0G_{\text{Ta}}^{\text{fcc}}$		${}^0G_{\text{Ta}}^{\text{bcc}}$		
$T_{\text{min}}, \text{K}$	298	3290	298	298	1300	2500	3290
$T_{\text{max}}, \text{K}$	3290	6000	6000	1300	2500	3290	6000
${}^0G^{\text{ref}}$	${}^0G_{\text{Ta}}^{\text{bcc}}$		-		-		-
$a_0$	29160.975	43884.339	16000	-7285.889	-22389.955	229382.886	-1042384.01
$a_1$	-7.578729	-61.981795	1.7	119.139857	243.88676	-722.59722	2985.49125
$a_2$	-	0.0279523	-	-23.7592624	-41.137088	78.5244752	-362.159132
$a_3$	-	-0.01233	-	-0.002623033	0.00616757	-0.0179833	0.043117795
$a_4$	-	$6.1459 \times 10^{-7}$	-	$1.70109 \times 10^{-7}$	$-6.551 \times 10^{-7}$	$1.9503 \times 10^{-7}$	$-1.055148 \times 10^{-6}$
$a_5$	-	-	-	-	-	-	-
$a_6$	-	-3523338	-	-3293	2429586	-93813648	$5.54714342 \times 10^8$
$a_7$	-	-	-	-	-	-	-
$a_8$	-	-	-	-	-	-	-

Note:  ${}^0G_i^\theta = a_0 + a_1T + a_2T \ln T + a_3T^2 + a_4T^3 + a_5T^4 + a_6T^{-1} + a_7T^{-9} + a_8T^7$  and  $T_c$  (K) is the Curie temperature and  $\beta$  is the average magnetic moment per atom (Bohr magnetons).

parameters  $\Delta G_{\text{Ni}_7\text{Ta}_6}^{\mu}$  (at  $\text{Ni}_7\text{Ta}_6$ ) and  $\Delta G_{\text{Ta}_7\text{Ta}_6}^{\mu}$  (at  $\text{Ni}_6\text{Ta}_7$ ) are selected first. These two parameters, however, are not sufficient to describe the composition range of the  $\mu$ -NiTa phase. To extend the composition range to left side, the parameter  $\Delta G_{\text{Ta}_7\text{Ta}_6}^{\mu}$  as well as the associated interaction parameter  ${}^0L_{\text{Ta}_7\text{Ta}_6}^{\mu}$  between end members  $\text{Ta}_1\text{Ta}_4\text{Ta}_2\text{Ni}_6$  and  $\text{Ta}_1\text{Ta}_4\text{Ta}_2\text{Ta}_6$  is included. Using the same arguments, the parameters  $\Delta G_{\text{Ni}_7\text{Ta}_6}^{\mu}$ ,  $\Delta G_{\text{Ta}_7\text{Ta}_6}^{\mu}$ , and  ${}^0L_{\text{Ta}_7\text{Ta}_6}^{\mu}$  are employed to extend composition range to right side. To accommodate the small solubility of Mo in the  $\mu$ -NiTa phase in ternary system, we modify this formulation to  $(\text{Ni}, \text{Ta})_1(\text{Ta})_4(\text{Mo}, \text{Ni}, \text{Ta})_2(\text{Ni}, \text{Ta})_6$ , permitting Mo on the third sublattice, and introduce the ternary parameters  $\Delta G_{\text{Ta}_7\text{Ta}_6}^{\mu}$  and  ${}^0L_{\text{Ta}_7\text{Ta}_6}^{\mu}$ . These parameters are sufficient for describing the  $\mu$ -NiTa phase, and the contributions from the remaining end members (i.e.  $G_{\text{Ni}_7\text{Ta}_6}^{\mu}$ ,  $G_{\text{Ta}_7\text{Ta}_6}^{\mu}$ ,  $G_{\text{Ni}_7\text{Ta}_6}^{\mu}$ ,  $G_{\text{Ta}_7\text{Ta}_6}^{\mu}$ ,  $G_{\text{Ni}_7\text{Ta}_6}^{\mu}$ ,  $G_{\text{Ta}_7\text{Ta}_6}^{\mu}$ ,  $G_{\text{Ni}_7\text{Ta}_6}^{\mu}$ , and  $G_{\text{Ta}_7\text{Ta}_6}^{\mu}$ ) listed in Table 3 are assumed to be zero.

The atoms in the  $\kappa$ - $\text{Ni}_3(\text{Mo}, \text{Ta})$ ,  $\text{C16-NiTa}_2$  and  $\text{C11b-Ni}_2\text{Ta}$  phases are distributed in two sublattices. The experimental data [6,7,10–12,15,16,28] reveal a homogeneous composition range for

these phases, and each is described here with a two-sublattice model, as shown in Table 3, where  $a_{ij}^\phi$ ,  $b_{ij}^\phi$ ,  ${}^0L_{i,lj}^\phi$  and  ${}^0L_{j,l}^\phi$  are the parameters to be evaluated.

Due to a lack of experimental data for  $\text{D0}_{22}\text{-Ni}_3\text{Ta}$ ,  $\zeta\text{-Ni}_8\text{Ta}$ , and  $\zeta\text{-Ni}_8\text{Mo}$ , these phases are treated as stoichiometric compounds in their respective binary systems. In the ternary Ni–Mo–Ta system, the experimental investigations by Chakravorty et al. [28] indicated a small solubility of Mo in  $\zeta\text{-Ni}_8\text{Ta}$ . Accordingly, the  $\zeta\text{-Ni}_8\text{Ta}$  and  $\zeta\text{-Ni}_8\text{Mo}$  phases are described here using a  $(\text{Ni})_8(\text{Mo}, \text{Ta})$  formulation, and the corresponding Gibbs free energy function is given in Table 3.

The  $\text{D0}_a\text{-Ni}_3\text{Mo}$  and  $\delta\text{-NiMo}$  phases are treated with a three-sublattice model using the formulation  $(\text{Mo}, \text{Ni})_4(\text{Ni})_2(\text{Mo}, \text{Ni})_2$  and  $(\text{Ni})_{24}(\text{Mo}, \text{Ni})_{20}(\text{Mo})_{12}$  as described in Ref. [8]. The experimental data by Chakravorty and West [28] and Cui et al. [9] revealed a small solubility of Ta in  $\text{D0}_a\text{-Ni}_3\text{Mo}$  and  $\delta\text{-NiMo}$ . These phases, denoted by  $\text{D0}_a\text{-Ni}_3(\text{Mo}, \text{Ta})$  and  $\delta\text{-NiMo}$ , are modeled here by considering the substitution of Ta for Mo, i.e.  $(\text{Mo}, \text{Ni}, \text{Ta})_4(\text{Ni})_2(\text{Mo}, \text{Ni}, \text{Ta})_2$  and  $(\text{Ni})_{24}(\text{Mo}, \text{Ni}, \text{Ta})_{20}(\text{Mo}, \text{Ta})_{12}$ , respectively, with the Gibbs free energy functions given in

**Table 3**Summary of the thermodynamic models used for the Ni–Mo–Ta ternary system with the total Gibbs free energy  $G_m^\phi = {}^{ref}G_m^\phi + {}^{id}G_m^\phi + {}^{xs}G_m^\phi$ .

Phase	Sublattice formulation	Model
Liquid fcc (A1) bcc (A2)	(Mo, Ni, Ta) <sub>1</sub>	${}^{ref}G_m^\phi = x_{Ni}^0 G_{Ni}^\phi + x_{Mo}^0 G_{Mo}^\phi + x_{Ta}^0 G_{Ta}^\phi$ ${}^{id}G_m^\phi = RT(x_{Ni} \ln x_{Ni} + x_{Mo} \ln x_{Mo} + x_{Ta} \ln x_{Ta})$ ${}^{xs}G_m^\phi = x_{Mo} x_{Ni} \sum_{j=0}^n {}^j L_{Mo,Ni}^\phi (x_{Mo} - x_{Ni})^j + x_{Mo} x_{Ta} \sum_{j=0}^n {}^j L_{Mo,Ta}^\phi (x_{Mo} - x_{Ta})^j$ $+ x_{Ni} x_{Ta} \sum_{j=0}^n {}^j L_{Ni,Ta}^\phi (x_{Ni} - x_{Ta})^j + x_{Mo} x_{Ni} x_{Ta} L_{Mo,Ni,Ta}^\phi$
$\mu$	(Ni, Ta) <sub>1</sub> (Ta) <sub>4</sub> (Mo, Ni, Ta) <sub>2</sub> (Ni, Ta) <sub>6</sub> Reference States: Group 1: Ni:Ta:Ni:Ni Ni:Ta:Ta:Ni Ta:Ta:Ni:Ni Ta:Ta:Ta:Ni Ta:Ta:Ta:Ta Ta:Ta:Mo:Ni Group 2: Ni:Ta:Ta:Ta Ta:Ta:Ni:Ta Ni:Ta:Ni:Ta Ta:Ta:Mo:Ta Ni:Ta:Mo:Ni Ni:Ta:Mo:Ta	${}^{ref}G_m^\mu = \sum_{i=Ni,Ta} y_i^I \sum_{j=Mo,Ni,Ta} y_j^{II} \sum_{k=Ni,Ta} y_k^{IV} G_{i:Ta;j:k}^{\mu}$ ${}^0 G_{i:Ta;j:k}^{\mu} = 0 {}^0 G_i^{fcc} + 4 {}^0 G_{Ta}^{bcc} + 2 {}^0 G_j^{bcc} + 6 {}^0 G_k^{fcc} + \Delta G_{i:Ta;j:k}^{\mu} (\text{Group 1})$ ${}^0 G_{i:Ta;j:k}^{\mu} = 0 (\text{Group 2})$ ${}^{id}G_m^\mu = RT \left( \sum_{i=Ni,Ta} (y_i^I \ln y_i^I + 2 y_i^{III} \ln y_i^{III} + 6 y_i^{IV} \ln y_i^{IV}) \right)$ ${}^{xs}G_m^\mu = y_{Ni}^I y_{Ta}^I \sum_{i=Mo,Ni,Ta} y_i^{II} \sum_{j=Ni,Ta} \sum_{k=0}^n {}^k L_{Ni,Ta:Ta;i;j}^{\mu} (y_{Ni}^I - y_{Ta}^I)^k$ $+ \sum_{i=Mo,Ni} \sum_{p=Ni,Ta} y_i^{III} y_p^{III} \sum_{j=Ni,Ta} \sum_{k=0}^n {}^k L_{i:Ta;l,p;j}^{\mu} (y_i^{III} - y_p^{III})^k$ $+ y_{Ni}^{IV} y_{Ta}^{IV} \sum_{i=Ni,Ta} \sum_{j=Mo,Ni,Ta} \sum_{k=0}^n {}^k L_{i:Ta;j:Ni,Ta}^{\mu} (y_{Ni}^{IV} - y_{Ta}^{IV})^k$
DO <sub>a</sub> I	(Mo, Ni, Ta) <sub>4</sub> (Ni) <sub>2</sub> (Mo, Ni, Ta) <sub>2</sub> Reference states: Group 1: Mo:Ni:Mo Ni:Ni:Mo Ta:Ni:Ta Ni:Ni:Ta Ni:Ni:Ni Group 2: (Mo, Ta):Ni:Ni Mo:Ni:Ta Ta:Ni:Mo	${}^{ref}G_m^{DO_a} = \sum_{i=Mo,Ni,Ta} y_i^I \sum_{j=Mo,Ni,Ta} y_j^{III} G_{i:Ni;j}^{DO_a}$ ${}^0 G_{i:Ni;j}^{DO_a} = 4 {}^0 G_i^{fcc} + 2 {}^0 G_{Ni}^{fcc} + 2 {}^0 G_j^{bcc} + \Delta G_{i:Ni;j}^{DO_a} (\text{Group 1})$ ${}^0 G_{i:Ni;j}^{DO_a} = 0 (\text{Group 2})$ ${}^{id}G_m^{DO_a} = RT \sum_{i=Mo,Ni,Ta} (4 y_i^I \ln y_i^I + 2 y_i^{III} \ln y_i^{III})$ ${}^{xs}G_m^{DO_a} = \sum_i \sum_{k>i} y_i^I y_k^I \sum_{j=Ni} \sum_{n=0}^n {}^n L_{i,k:Ni;j}^{DO_a} (y_i^I - y_k^I)^n$ $+ \sum_j \sum_i \sum_{k>i} y_i^{III} y_k^{III} \sum_{n=0}^n {}^n L_{i:Ni;k}^{DO_a} (y_i^{III} - y_k^{III})^n$
$\kappa$ DO <sub>a</sub> II C16 C11 <sub>b</sub> $\zeta$	(Ni, Mo, Ta) <sub>3</sub> (Ni, Mo, Ta) <sub>1</sub> Note: ${}^0 G_{Mo:Ta}^{DO_aII} = {}^0 G_{Ta:Mo}^{DO_aII} = 0$ (Ni, Ta) <sub>1</sub> (Ni, Ta) <sub>2</sub> (Ni, Ta) <sub>2</sub> (Ni, Ta) <sub>1</sub> (Ni) <sub>8</sub> (Mo, Ta)	${}^{ref}G_m^\phi = \sum_{i=Mo,Ni,Ta} y_i^I \sum_{j=Mo,Ni,Ta} y_j^{II} G_{i;j}^\phi$ ${}^0 G_{i;j}^\phi = p {}^0 G_i^{ref} + q {}^0 G_j^{ref} + \Delta G_{i;j}^\phi = p {}^0 G_i^{ref} + q {}^0 G_j^{ref} + a_{ij}^\phi + b_{ij}^\phi T$ ${}^{id}G_m^\phi = RT \sum_{i=Mo,Ni,Ta} (p y_i^I \ln y_i^I + q y_i^{II} \ln y_i^{II})$ ${}^{xs}G_m^\phi = \sum_i \sum_{l>i} y_i^I y_l^I \sum_j \sum_{k=0}^n {}^k L_{i,l;j}^\phi (y_i^I - y_l^I)^k$ $+ \sum_j \sum_i \sum_{l>i} y_i^{II} y_l^{II} \sum_{k=0}^n {}^k L_{j;l,i}^\phi (y_i^{II} - y_l^{II})^k$ <p>(<math>p</math> and <math>q</math> are the subscript numbers of sublattices, respectively)</p>
$\delta$	(Ni) <sub>24</sub> (Mo, Ni, Ta) <sub>20</sub> (Mo, Ta) <sub>12</sub>	${}^{ref}G_m^\delta = \sum_{i=Mo,Ni,Ta} y_i^I \sum_{j=Mo,Ta} y_j^{III} G_{Ni:i;j}^\delta$ ${}^0 G_{Ni:i;j}^\delta = 24 {}^0 G_{Ni}^{fcc} + 20 {}^0 G_i^{bcc} + 12 {}^0 G_j^{bcc} + \Delta G_{Ni:i;j}^\delta$ ${}^{id}G_m^\delta = RT \left( \sum_{i=Ni,Ta} (20 y_i^I \ln y_i^I + 12 y_i^{III} \ln y_i^{III}) \right)$ ${}^{xs}G_m^\delta = \sum_{i=Mo,Ni} \sum_{j=Ni,Ta} y_i^I y_j^{III} \sum_{k=0}^n {}^k L_{Ni:i,j;l}^\delta (y_i^I - y_j^{III})^k$ $+ \sum_{i=Mo,Ni,Ta} y_i^{III} y_{Mo}^{III} \sum_{k=0}^n {}^k L_{Ni:i:Mo,Ta}^\delta (y_{Mo}^{III} - y_i^{III})^k$
Ni <sub>2</sub> Mo Ni <sub>4</sub> Mo DO <sub>22</sub>	(Ni) <sub>2</sub> (Mo) <sub>1</sub> (Ni) <sub>4</sub> (Mo) <sub>1</sub> (Ni) <sub>3</sub> (Ta) <sub>1</sub>	$G_m^\phi = \Delta G_{Ni:Ta}^\phi + p {}^0 G_{Ni}^{fcc} + q {}^0 G_{i(i=Mo,Ta)}^{bcc}$ $= a^\phi + b^\phi T + p {}^0 G_{Ni}^{fcc} + q {}^0 G_{i(i=Mo,Ta)}^{bcc}$ <p>(<math>p</math> and <math>q</math> are the subscript numbers of sublattices, respectively)</p>

**Table 3.** DO<sub>a</sub>-Ni<sub>3</sub>Mo was also described with the two-sublattice model using the (Mo, Ni)<sub>3</sub>(Mo, Ni)<sub>1</sub> formulation in Ref. [8]. To be compatible with this treatment in the ternary system, another set of parameters is developed for the two-sublattice model, i.e. (Mo, Ni, Ta)<sub>3</sub>(Mo, Ni, Ta)<sub>1</sub>, denoted by DO<sub>a</sub>II-Ni<sub>3</sub>(Mo, Ta). In this case, the Gibbs free energy functions can be written in the same form as those for  $\kappa$ -Ni<sub>3</sub>(Mo, Ta) in Table 3.

### 3. Determination of the thermodynamic model parameters

In the determination of the model parameters for the ternary Ni–Mo–Ta system, the Ni–Ta binary is evaluated first and then integrated with reported models for the Ni–Mo [8] in Fig. 1(d) and Mo–Ta [9] in Fig. 1(e) systems to build the thermodynamic description. With the thermodynamic models described in the preceding section, we employ a total of twenty-four Gibbs

free energy of formation parameters and fourteen interaction parameters for the binary Ni–Ta system, as listed in Tables 4 and 5. The evaluation process, utilizing both experimental data and first principles results for the Ni–Ta system, is discussed in this section.

Using VASP [38] with the Vanderbilt ultrasoft pseudopotential [39] within the generalized gradient approximation (GGA) [40], the total energy of the fcc-Ni, bcc-Mo, bcc-Ta, and compounds are calculated. Monkhorst 15 × 15 × 15  $k$  points are used for the pure elements Ni, Mo and Ta, 11 × 11 × 11  $k$  points for the end-members of the  $\zeta$ -Ni<sub>8</sub>Ta, DO<sub>22</sub>-Ni<sub>3</sub>Ta, C11<sub>b</sub>-Ni<sub>2</sub>Ta, DO<sub>a</sub>-Ni<sub>3</sub>Mo and C16-NiTa<sub>2</sub> phases, 9 × 9 × 9  $k$  points for the end-members of the  $\mu$ -NiTa phase and 4 × 4 × 4  $k$  points for the end-members of the  $\kappa$ -Ni<sub>3</sub>Ta phase. To ensure that the unit cell corresponds to a stable structure, we fully relax the cell shape and the internal atomic coordinates for the stable end-members and relax only the cell volume for the unstable/metastable end-members.

**Table 4**  
Gibbs free energy of formation for end-member reference states (per mole of formula unit).

Phase	Parameter	Value (J/mol)	Ref.
C16	$\Delta G_{Ni;Ni}^{C16}$	80310	
	$\Delta G_{Ta;Ni}^{C16}$	132420	
	$\Delta G_{Ni;Ta}^{C16}$	$-65550 + 6.246T$	
	$\Delta G_{Ta;Ta}^{C16}$	152640	
$\mu$	$\Delta G_{Ni;Ta;Ni;Ni}^{\mu}$	-167960	
	$\Delta G_{Ta;Ta;Ni;Ni}^{\mu}$	-149240	
	$\Delta G_{Ni;Ta;Ta;Ni}^{\mu}$	-298870	
	$\Delta G_{Ta;Ta;Ta;Ni}^{\mu}$	$-356630 + 24.003T$	
	$\Delta G_{Ta;Ta;Ta;Ta}^{\mu}$	221650	
	$\Delta G_{Ta;Ta;Mo;Ni}^{\mu}$	-320230	
C11 <sub>b</sub>	$\Delta G_{Ni;Ni}^{C11_b}$	23730	Present
	$\Delta G_{Ta;Ni}^{C11_b}$	15000	
	$\Delta G_{Ni;Ta}^{C11_b}$	$-110001 + 20.919T$	
	$\Delta G_{Ta;Ta}^{C11_b}$	31470	
$\kappa$	$\Delta G_{Ni;Ni}^{\kappa}$	14000	
	$\Delta G_{Ni;Ta}^{\kappa}$	$-122760 + 11.692T$	
	$\Delta G_{Ta;Ni}^{\kappa}$	50160	
	$\Delta G_{Ta;Ta}^{\kappa}$	117280	
	$\Delta G_{Ta;Mo}^{\kappa}$	128320	
	$\Delta G_{Mo;Ta}^{\kappa}$	146400	
	$\Delta G_{Mo;Mo}^{\kappa}$	164360	
	$\Delta G_{Ni;Mo}^{\kappa}$	$-15440 + 74.112T - 9.823807\ln(T)$	
DO <sub>a</sub> -I	$\Delta G_{Ta;Ni;Ta}^{DO_a}$	99840	Present
	$\Delta G_{Ni;Ni;Ta}^{DO_a}$	$-275040 + 74.368T$	Present
	$\Delta G_{Mo;Ni;Mo}^{DO_a}$	136480	[8]
	$\Delta G_{Ni;Ni;Mo}^{DO_a}$	$-81055.2 + 465.054T - 58.929T\ln(T)$	[8]
DO <sub>a</sub> -II	$\Delta G_{Ta;Ta}^{DO_aII}$	123200	Present
	$\Delta G_{Ni;Ta}^{DO_aII}$	$\Delta G_{Ni;Ni;Ta}^{DO_a} / 2$	Present
	$\Delta G_{Ta;Ni}^{DO_aII}$	$\Delta G_{Ta;Ni;Ta}^{DO_a} / 2$	Present
	$\Delta G_{Mo;Mo}^{DO_aII}$	170600	[8]
	$\Delta G_{Ni;Mo}^{DO_aII}$	$\Delta G_{Ni;Ni;Mo}^{DO_a} / 2$	[8]
	$\Delta G_{Mo;Ni}^{DO_aII}$	$\Delta G_{Mo;Ni;Mo}^{DO_a} / 2$	[8]
	$\Delta G_{Ni;Ni}^{DO_aII}$	$\Delta G_{Ni;Ni;Ni}^{DO_a} / 2$	[8]
	$\Delta G_{Ni;Ta}^{\zeta}$	$-162918 + 20.736T$	Present
$\zeta$	$\Delta G_{Ni;Mo}^{\zeta}$	$-55035 + 299.322T - 36.765T\ln(T)$	[8]
	$\Delta G_{Ni;Mo;Mo}^{\delta}$	$-169981 + 1154.981T - 155.484T\ln(T)$	[8]
$\delta$	$\Delta G_{Ni;Ni;Mo}^{\delta}$	$-154106 + 2855.001T - 394.923T\ln(T)$	[8]
	$\Delta G_{Ni;Ta;Mo}^{\delta}$	-1224888	Present
	$\Delta G_{Ni;Mo;Ta}^{\delta}$	-679392	Present
	$\Delta G_{Ni;Ni;Ta}^{\delta}$	-1203776	Present
	$\Delta G_{Ni;Ta;Ta}^{\delta}$	34496	Present
	Ni <sub>2</sub> Mo	$\Delta G_{Ni;Mo}^{Ni_2Mo}$	$-28263 + 148.653T - 18.693T\ln(T)$
Ni <sub>4</sub> Mo	$\Delta G_{Ni;Mo}^{Ni_4Mo}$	$-45105 + 275.020T - 35.400T\ln(T)$	[8]
DO <sub>22</sub>	$\Delta G_{Ni;Ta}^{DO_{22}}$	$-146360 + 50.804T$	Present

The enthalpy of formation  $\Delta H_f^\Phi$  for a given compound  $\Phi$  is calculated as the difference between the energy  $E_{TOT}^\Phi$  of the compound and linear combination of the pure element reference state energies,  $E_{Ni}^{fcc}$ ,  $E_{Mo}^{bcc}$  and  $E_{Ta}^{bcc}$ ,

$$\Delta H_f^\Phi = E_{TOT}^\Phi - x_{Ni}^\Phi E_{Ni}^{fcc} - x_{Ta}^\Phi E_{Ta}^{bcc} - x_{Mo}^\Phi E_{Mo}^{bcc} \quad (2)$$

where  $x_i^\Phi$  is the mole fraction of component  $i$  in  $\Phi$ . The calculated enthalpies of formation are plotted in Fig. 2 and listed in Table 6.

The first principles calculations yielded two important results, both shown in Fig. 2. First, it was found that  $\mu$ -NiTa is not stable at 0 K relative to the compounds C16-NiTa<sub>2</sub> and C11<sub>b</sub>-Ni<sub>2</sub>Ta. Second, the compound DO<sub>22</sub>-Ni<sub>3</sub>Ta was found to be stable at 0 K

**Table 5**  
Excess Gibbs free energy interaction parameters.

Phase	Parameters	Value (J/mol)	Ref.
Liquid	${}^0L_{Ni;Ta}^{liq}$	-83812	Present
	${}^1L_{Ni;Ta}^{liq}$	-46039	
	${}^2L_{Ni;Ta}^{liq}$	-4023	
	${}^0L_{Mo;Ta}^{liq}$	-73477	[9]
	${}^1L_{Mo;Ta}^{liq}$	-4091	
		${}^0L_{Mo;Ni}^{liq}$	$-39597 + 15.935T$
${}^1L_{Mo;Ni}^{liq}$		$-7373 + 4.102T$	
${}^2L_{Mo;Ni}^{liq}$		$-12123 + 5.551T$	
Bcc		${}^0L_{Ni;Ta}^{bcc}$	$-28415 - 10.613T$
	${}^1L_{Ni;Ta}^{bcc}$	-32471	
	${}^0L_{Mo;Ta}^{bcc}$	-69360	[9]
	${}^1L_{Mo;Ta}^{bcc}$	-4190	
	${}^0L_{Mo;Ni}^{bcc}$	27691	[8]
	${}^1L_{Mo;Ni}^{bcc}$	18792	
	${}^0L_{Mo;Ni;Ta}^{bcc}$	$-140353 + 59.354T$	Present
	${}^1L_{Mo;Ni;Ta}^{bcc}$	28573	
	${}^2L_{Mo;Ni;Ta}^{bcc}$	$-126245 + 73.235T$	
	Fcc	${}^0L_{Ni;Ta}^{fcc}$	$-75470 - 4.023T$
${}^1L_{Ni;Ta}^{fcc}$		$-71135 + 13.235T$	
${}^2L_{Ni;Ta}^{fcc}$		-6572	
${}^0L_{Mo;Ni}^{fcc}$		$-8916 + 3.591T$	[8]
${}^1L_{Mo;Ni}^{fcc}$		$5469 - 0.249T$	
${}^2L_{Mo;Ni}^{fcc}$		$-1549 - 2.741T$	
C16	${}^0L_{Ni;Ni;Ta}^{C16}$	45410	Present
	${}^1L_{Ni;Ni;Ta}^{C16}$	$-20214 - 27.435T$	
	${}^2L_{Ni;Ni;Ta}^{C16}$	-45001	
	${}^0L_{Ni;Ta;Ta}^{C16}$	$-190695 + 46.446T$	
$\mu$	${}^0L_{Ta;Ni;Ta;Ni}^{\mu}$	$-377513 + 70.302T$	Present
	${}^0L_{Ta;Ta;Ni;Ta}^{\mu}$	$-405208 + 50.923T$	
	${}^0L_{Ta;Ta;Mo;Ta;Ni}^{\mu}$	-71310	
C11 <sub>b</sub>	${}^0L_{Ni;Ni;Ta}^{C11_b}$	-58029	
$\kappa$	${}^0L_{Ni;Ni;Ta}^{\kappa}$	$-42372 + 30.436T$	Present
	${}^0L_{Ni;Ta;Ta}^{\kappa}$	$-42373.6 + 40.516T$	
	${}^0L_{Mo;Ni;Mo}^{\kappa}$	-14045.5	
	${}^0L_{Ni;Mo;Ta}^{\kappa}$	$-32440 + 11.428T$	
DO <sub>a</sub> -I	${}^0L_{Ni;Ni;Mo}^{DO_a}$	-10804	[8]
	${}^0L_{Ni;Mo;Ta}^{DO_a}$	$-69324 - 208456 + 127.928T$	
DO <sub>a</sub> -II	${}^0L_{Mo;Ni;Mo}^{DO_aII}$	-26840	[8]
	${}^0L_{Ni;Mo;Ni}^{DO_aII}$	$4792 - 1.604T$	[8]
	${}^0L_{Ni;Mo;Ta}^{DO_aII}$	${}^0L_{Ni;Ni;Mo;Ta}^{DO_a} / 2$	Present
$\zeta$	${}^0L_{Ni;Mo;Ta}^{\zeta}$	-17802	Present
$\delta$	${}^0L_{Ni;Mo;Ni;Mo}^{\delta}$	$-829211 + 825.923T$	[8]
	${}^1L_{Ni;Mo;Ni;Mo}^{\delta}$	$-417368.2 + 326.504T$	

with respect to  $\kappa$ -Ni<sub>3</sub>Ta, with an energy difference of 6 kJ/mole (atoms). In contrast, the experimental data [6,7,10–12,15,16] in Fig. 1 show that the compound  $\kappa$ -Ni<sub>3</sub>Ta is stable at high temperatures. Without specific experimental data indicating the exact temperature of the transition, we assume a temperature of 600 K for the transition from the high temperature stable compound  $\kappa$ -Ni<sub>3</sub>Ta (i.e.  $\kappa$ -Ni<sub>3</sub>(Mo, Ta) [6,7,10–12,15,16] to the low temperature stable DO<sub>22</sub>-Ni<sub>3</sub>Ta phase.

The parameter evaluation process for the Ni-Ta system is started with the liquid phase followed by  $\kappa$ -Ni<sub>3</sub>Ta, fcc and bcc and the compounds,  $\zeta$ -Ni<sub>8</sub>Ta, C11<sub>b</sub>-Ni<sub>2</sub>Ta, C16-NiTa<sub>2</sub> and  $\mu$ -NiTa. Due to the significant difference between the experimental data by Sudavtsova [19] and Schaeffers [20], shown in Fig. 3, two sets of parameters for the liquid phase are determined. To select the

**Table 6**

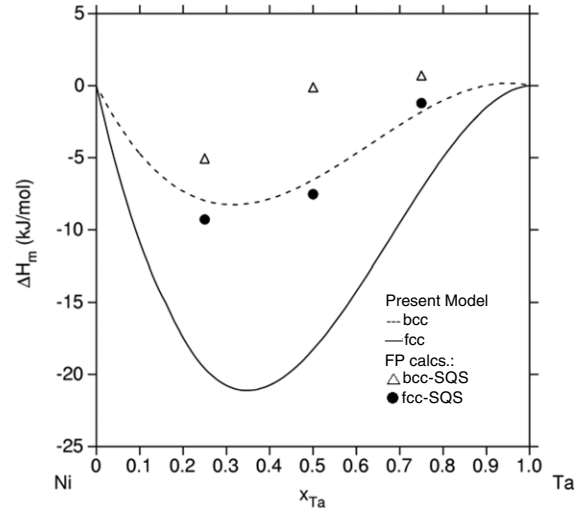
A summary of results from the first-principles calculations.

Phase	Symbol	Prototype	Formula	$\Delta H$ , (kJ/mol)
Ni	A1	fcc	Ni	0
	A2	bcc	Ni	9.33
Mo	A2	bcc	Mo	0
	A1	fcc	Mo	39.51
Ta	A1	fcc	Ta	26.23
	A2	bcc	Ta	0
Ni <sub>0.25</sub> Ta <sub>0.75</sub> <sup>a</sup>	A2	bcc-SQS16	Ni <sub>0.25</sub> Ta <sub>0.75</sub>	0.588
			Ni <sub>0.50</sub> Ta <sub>0.50</sub> <sup>a</sup>	-0.23
			Ni <sub>0.75</sub> Ta <sub>0.25</sub> <sup>a</sup>	-5.17
Ni <sub>0.25</sub> Ta <sub>0.75</sub> <sup>b</sup>	A1	fcc-SQS16	Ni <sub>0.25</sub> Ta <sub>0.75</sub>	-12.16
			Ni <sub>0.50</sub> Ta <sub>0.50</sub> <sup>b</sup>	-7.54
			Ni <sub>0.75</sub> Ta <sub>0.25</sub> <sup>b</sup>	-9.28
NiTa <sub>2</sub>	C16	Al <sub>2</sub> Cu [33]	Ni <sub>1</sub> Ni <sub>2</sub>	26.77
			Ta <sub>1</sub> Ni <sub>2</sub>	44.14
			Ni <sub>1</sub> Ta <sub>2</sub>	-21.15
			Ta <sub>1</sub> Ta <sub>2</sub>	50.88
NiTa	$\mu$	Fe <sub>7</sub> W <sub>6</sub> [33]	NiTa <sub>4</sub> Ni <sub>2</sub> Ni <sub>6</sub>	-12.92
			TaTa <sub>4</sub> Ni <sub>2</sub> Ni <sub>6</sub>	-18.61
			NiTa <sub>4</sub> Ta <sub>2</sub> Ni <sub>6</sub>	-22.99
			TaTa <sub>4</sub> Ta <sub>2</sub> Ni <sub>6</sub>	-25.51
			TaTa <sub>4</sub> Ta <sub>2</sub> Ta <sub>6</sub>	17.05
			TaTa <sub>4</sub> Mo <sub>2</sub> Ni <sub>6</sub>	-17.52
Ni <sub>2</sub> Ta	C11 <sub>b</sub>	MoSi <sub>2</sub> [26]	Ni <sub>2</sub> Ni	7.91
			Ni <sub>2</sub> Ta	-32.36
			Ta <sub>2</sub> Ni	5.00
			Ta <sub>2</sub> Ta	10.49
NiMo	$\delta$	NiMo	Ni <sub>24</sub> Ta <sub>20</sub> Mo <sub>12</sub>	-16.79
			Ni <sub>24</sub> Mo <sub>20</sub> Ta <sub>12</sub>	-10.08
			Ni <sub>24</sub> Ni <sub>20</sub> Ta <sub>12</sub>	-16.48
			Ni <sub>24</sub> Ta <sub>20</sub> Ta <sub>12</sub>	0.62
Ni <sub>3</sub> Ta	$\kappa$	Pt <sub>3</sub> Ta [26]	Ni <sub>3</sub> Ni	3.50
			Ni <sub>3</sub> Ta	-29.29
			Ta <sub>3</sub> Ni	12.54
			Ta <sub>3</sub> Ta	29.32
			Ta <sub>3</sub> Mo	32.08
			Mo <sub>3</sub> Ta	36.6
			Mo <sub>3</sub> Mo	41.09
	Ni <sub>3</sub> Mo	-1.86		
	Mo <sub>3</sub> Ni	18.85		
	DO <sub>a</sub>	Cu <sub>3</sub> Ti [26]	Ta <sub>3</sub> Ta	Ni <sub>3</sub> Ta
Ta <sub>3</sub> Ni				12.48
Ta <sub>3</sub> Ta				30.80
DO <sub>22</sub>	Al <sub>3</sub> Ti [26]	Ni <sub>3</sub> Ta	-35.29	
Ni <sub>8</sub> Ta	$\zeta$	Nb <sub>8</sub> Ni [14]	Ni <sub>8</sub> Ta	-16.37

<sup>a</sup> Reference states: Ni-bcc and Ta-bcc.<sup>b</sup> Reference states: Ni-fcc and Ta-fcc.

more appropriate parameter set, the parameters for  $\kappa$ -Ni<sub>3</sub>(Mo, Ta) are evaluated next. The reason is that the parameters,  $a_{\text{Ni:Ta}}^{\kappa}$  and  $b_{\text{Ni:Ta}}^{\kappa}$ , are fixed with the first-principles data and the melting temperature of  $\kappa$ -Ni<sub>3</sub>(Mo, Ta), while the phase equilibrium data liq/liq +  $\kappa$ -Ni<sub>3</sub>(Mo, Ta) [10–13] are used to examine the reliability of the liquid parameters. The results indicate that the parameters evaluated from the data by Sudavtsova [19] better reproduce the liquidus for  $\kappa$ -Ni<sub>3</sub>(Mo, Ta) [10–13] than do those from the data by Schaefer [20], and the Sudavtsova data [19] are selected for use in the current model description. In addition to  $a_{\text{Ni:Ta}}^{\kappa}$  and  $b_{\text{Ni:Ta}}^{\kappa}$ , the parameters  $a_{ij}^{\kappa}$  and  ${}^0L^{\kappa}$  for  $\kappa$ -Ni<sub>3</sub>(Mo, Ta) are evaluated with the first-principles results and reported phase diagram data [6,7,10–13,15].

The enthalpies of mixing for the bcc and fcc solution phases are calculated using three 16-atom SQS [23,24,41] for compositions of



**Fig. 4.** The enthalpy of mixing, as computed using the present model, for the bcc solution (referenced to bcc-Ni and bcc-Ta) and fcc solution (referenced to fcc-Ni and fcc-Ta).

$x_{\text{Ni}} = 0.25, 0.5, \text{ and } 0.75$ , respectively. Using the same arguments as that for the unstable end-members of the multi-sublattice models, we only relax the cell volume of the SQS without local lattice relaxations. The calculated enthalpies of mixing of the SQS for both bcc and fcc are listed in Table 6 and plotted in Fig. 4. To evaluate the parameters for the fcc and bcc solutions, both the phase equilibrium data [6,7,10,12–16] and the first-principles calculated enthalpies of mixing in Table 6 are considered. Similar to the procedure described above for the liquid and  $\kappa$ -Ni<sub>3</sub>(Mo, Ta) phases, the parameters  $a_{\text{Ni:Ta}}^{\zeta}$  and  $b_{\text{Ni:Ta}}^{\zeta}$  for  $\zeta$ -Ni<sub>8</sub>(Mo, Ta) are determined using the first-principles results and the congruent phase transformation temperature of  $\zeta$ -Ni<sub>8</sub>Ta [15,16], and the experimental data for the fcc/fcc +  $\zeta$ -Ni<sub>8</sub>Ta solvus [6,7,12,13] are subsequently used to determine the fcc parameters.

The parameters  $a_{ij}^{\text{C11b}}$ ,  $a_{\text{Ni:Ta}}^{\text{DO}_{22}}$ ,  $a_{ij}^{\text{C16}}$ ,  $a_{\text{Ta:Ta:Ta:Ta}}^{\mu}$  and  $a_{\text{Ta:Ta:Ta:Ta}}^{\mu}$  are fixed by the first-principles data and the experimental enthalpy of formation [22], as shown in Fig. 2. The parameters  $b_{\text{Ni:Ta}}^{\text{C11b}}$ ,  $b_{\text{Ni:Ta}}^{\text{C16}}$  and  $b_{\text{Ta:Ta:Ta:Ta}}^{\mu}$  and interaction parameters  ${}^0L^{\text{C11b}}$ ,  ${}^0L^{\text{C16}}$ ,  ${}^0L^{\text{C16}}$ ,  ${}^0L^{\text{C16}}$ ,  ${}^0L^{\mu}$  and  ${}^0L^{\mu}$  are evaluated with the phase equilibrium data [6,7,10–12,15]. The parameter  $b_{\text{Ni:Ta}}^{\text{DO}_{22}}$  is evaluated by assuming that the phase transformation  $\kappa$ -Ni<sub>3</sub>Ta → DO<sub>22</sub>-Ni<sub>3</sub>Ta occurs at 600 K, which can be modified when experimental data become available. The practice is iterative and culminates with an optimized fit involving all available data and calculation results. The overall optimization results are summarized in Tables 4 and 5.

For the Ni–Mo–Ta ternary system, the models for the binary Ni–Ta system described above are combined with reported treatments for the Ni–Mo [8] and Mo–Ta [9] systems, summarized in Tables 4 and 5, respectively. The ternary parameters are evaluated in the order of fcc,  $\kappa$ -Ni<sub>3</sub>(Mo, Ta), DO<sub>a</sub>-Ni<sub>3</sub>(Mo, Ta),  $\zeta$ -Ni<sub>8</sub>(Mo, Ta),  $\mu$ -NiTa, and bcc, based on the availability of experimental data.

The solubility of Mo in  $\kappa$ -Ni<sub>3</sub>(Mo, Ta) was experimentally determined by Cui et al. [9], Virkar and Raman [27], and Chakravorty and West [28], indicating that Mo dissolves into  $\kappa$ -Ni<sub>3</sub>Ta up to 6 at.% Mo at 1173 K. The Gibbs free energy terms,  $\Delta G_{\text{Mo:Mo}}^{\kappa}$ ,  $\Delta G_{\text{Ni:Mo}}^{\kappa}$ ,  $\Delta G_{\text{Mo:Ni}}^{\kappa}$ ,  $\Delta G_{\text{Mo:Ta}}^{\kappa}$ ,  $\Delta G_{\text{Ta:Mo}}^{\kappa}$ , and the interaction parameters,  ${}^0L_{\text{Mo,Ni:Mo}}^{\kappa}$  and  ${}^0L_{\text{Ni,Mo:Ta}}^{\kappa}$ , are used here to extend the single  $\kappa$ -Ni<sub>3</sub>Ta composition range toward the Ni–Mo edge.  $\Delta G_{\text{Mo:Mo}}^{\kappa}$ ,  $\Delta G_{\text{Ni:Mo}}^{\kappa}$ ,  $\Delta G_{\text{Mo:Ni}}^{\kappa}$ ,  $\Delta G_{\text{Mo:Ta}}^{\kappa}$ , and  $\Delta G_{\text{Ta:Mo}}^{\kappa}$  are assumed to be constant and fixed with the first-principles data. The parameters

**Table 7**  
Invariant reactions in the Ni–Ta system.

Reaction	Calculated results	Experimental Results (K)			
		This work	[6]	[7]	
liq + bcc → C16-NiTa <sub>2</sub>	T, K	2060	2067	2051	2061 [12]
	x(liq, Ta)	0.551	0.595	0.559	
	x(bcc, Ta)	0.791	0.788	0.799	
	x(C16, Ta)	0.708	0.692	0.711	
liq + C16Ta <sub>2</sub> → μ-NiTa	T, K	1842	1842	1851	1844 [10]
	x(liq, Ta)	0.471	0.493	0.486	1817–1847 [11]
	x(C16, Ta)	0.679	0.667	0.674	1843 [12]
	x(μ, Ta)	0.574	0.531	0.530	
liq → κ-Ni <sub>3</sub> Ta	T, K	1805	1810	1824	1814 [10]
	x(liq, Ta)	0.25	0.25	0.25	1815 [11]
	x(κ, Ta)	0.25	0.25	0.25	1808 [12]
liq → fcc + κ-Ni <sub>3</sub> Ta	T, K	1666	1627	1625	1616–1639 [10]
	x(liq, Ta)	0.144	0.139	0.153	1643 [11]
	x(fcc, Ta)	0.137	0.113	0.139	1633 [12]
	x(κ, Ta)	0.241	0.230	0.242	
liq + κ-Ni <sub>3</sub> Ta → C11 <sub>b</sub> -Ni <sub>2</sub> Ta	T, K	1678	1676	1662	1618–1664 [10]
	x(liq, Ta)	0.366	0.355	0.357	1673 [11]
	x(κ, Ta)	0.253	0.271	0.279	1678 [12]
	x(C11 <sub>b</sub> , Ta)	0.344	0.333	0.341	
liq → μ-NiTa + C11 <sub>b</sub> -Ni <sub>2</sub> Ta	T, K	1678	1663	1647	1615–1661 [10]
	x(liq, Ta)	0.367	0.373	0.381	1639 [11]
	x(μ, Ta)	0.502	0.500	0.504	1634 [12]
	x(C11 <sub>b</sub> , Ta)	0.344	0.333	0.349	
fcc → ζ-Ni <sub>8</sub> Ta	T, K	1584	1581	1584	1573 [15]
	x(liq, Ta)	0.111	0.111	0.111	1593 [16]
	x(κ, Ta)	0.111	0.111	0.111	
fcc → κ-Ni <sub>3</sub> Ta + ζ-Ni <sub>8</sub> Ta	T, K	1571	1580	1547	
	x(fcc, Ta)	0.126	0.1114	0.136	1572 [13]
	x(κ, Ta)	0.237	0.231	0.242	
	x(ζ, Ta)	0.111	0.1111	0.111	
κ-Ni <sub>3</sub> Ta + C11 <sub>b</sub> -Ni <sub>2</sub> Ta → D0 <sub>22</sub> -Ni <sub>3</sub> Ta	T, K	603	–	–	–
	x(κ, Ta)	0.249(9)	–	–	–
	x(D0 <sub>22</sub> , Ta)	0.25	–	–	–
	x(C11 <sub>b</sub> , Ta)	0.329	–	–	–
κ-Ni <sub>3</sub> Ta → D0 <sub>22</sub> -Ni <sub>3</sub> Ta + ζ-Ni <sub>8</sub> Ta	T, K	600	–	–	–
	x(κ, Ta)	0.244	–	–	–
	x(D0 <sub>22</sub> , Ta)	0.25	–	–	–
	x(ζ, Ta)	0.111	–	–	–
μ-NiTa → C16-NiTa <sub>2</sub> + C11 <sub>b</sub> -Ni <sub>2</sub> Ta	T, K	474	–	109	–
	x(μ, Ta)	0.526	–	0.504	–
	x(C16, Ta)	0.666	–	0.667	–
	x(C11 <sub>b</sub> , Ta)	0.334	–	0.333	–
κ-Ni <sub>3</sub> Ta → ζ-Ni <sub>8</sub> Ta + C11 <sub>b</sub> -Ni <sub>2</sub> Ta	T, K	–	231	42	–
	x(κ, Ta)	–	0.25	0.25	–
	x(ζ, Ta)	–	0.111	0.111	–
	x(C11 <sub>b</sub> , Ta)	–	0.333	0.333	–

$i_L^{fcc}$ ,  $b_{Ni,Mo,Ta}^{Ni,Mo,Ta}$ ,  $b_{Ni,Mo}^{Ni,Mo}$ ,  $L_{Mo,Ni:Mo}^{Ni,Mo}$ ,  $L_{Ni:Mo,Ta}^{Ni,Mo}$  and  $L_{Ni,Mo:Ta}^{Ni,Mo}$  are evaluated with the phase equilibrium data [9,27,28], as listed in Tables 4 and 5.

The parameters for the D0<sub>a</sub>-Ni<sub>3</sub>Mo phase are determined using the same methodology as described above for the κ-Ni<sub>3</sub>(Mo, Ta) phase. Selected parameters ( $\Delta G_{Ta:Ni:Ta}^{D0_a}$ ,  $\Delta G_{Ni:Ni:Ta}^{D0_a}$ ,  $\Delta G_{Ta:Ta}^{D0_a}$ ,  $\Delta G_{Ta:Ni}^{D0_a}$ ,  $\Delta G_{Ni:Mo,Ta}^{D0_a}$ ,  $\Delta G_{Ni:Mo,Ta}^{D0_a}$ ) are utilized to model the experimentally observed solubility of Ta, reported by Chakravorty and West [28]. Accordingly, these parameters are adjusted to extend the D0<sub>a</sub>-Ni<sub>3</sub>Mo composition range toward the Ni–Ta binary. The parameters  $\Delta G_{Ta:Ni:Ta}^{D0_a}$ ,  $\Delta G_{Ni:Ni:Ta}^{D0_a}$ ,  $\Delta G_{Ta:Ta}^{D0_a}$ ,  $\Delta G_{Ta:Ni}^{D0_a}$  and  $\Delta G_{Ni:Mo,Ta}^{D0_a}$  are considered as constant and fixed with the first-principles data, while  $b_{Ni:Mo,Ta}^{D0_a}$ ,  $b_{Ni:Ta}^{D0_a}$ ,  $b_{Ni:Mo,Ta}^{D0_a}$  and  $b_{Ni:Mo,Ta}^{D0_a}$  are evaluated with reported phase boundary data for D0<sub>a</sub>-Ni<sub>3</sub>Mo [28]. For the δ-

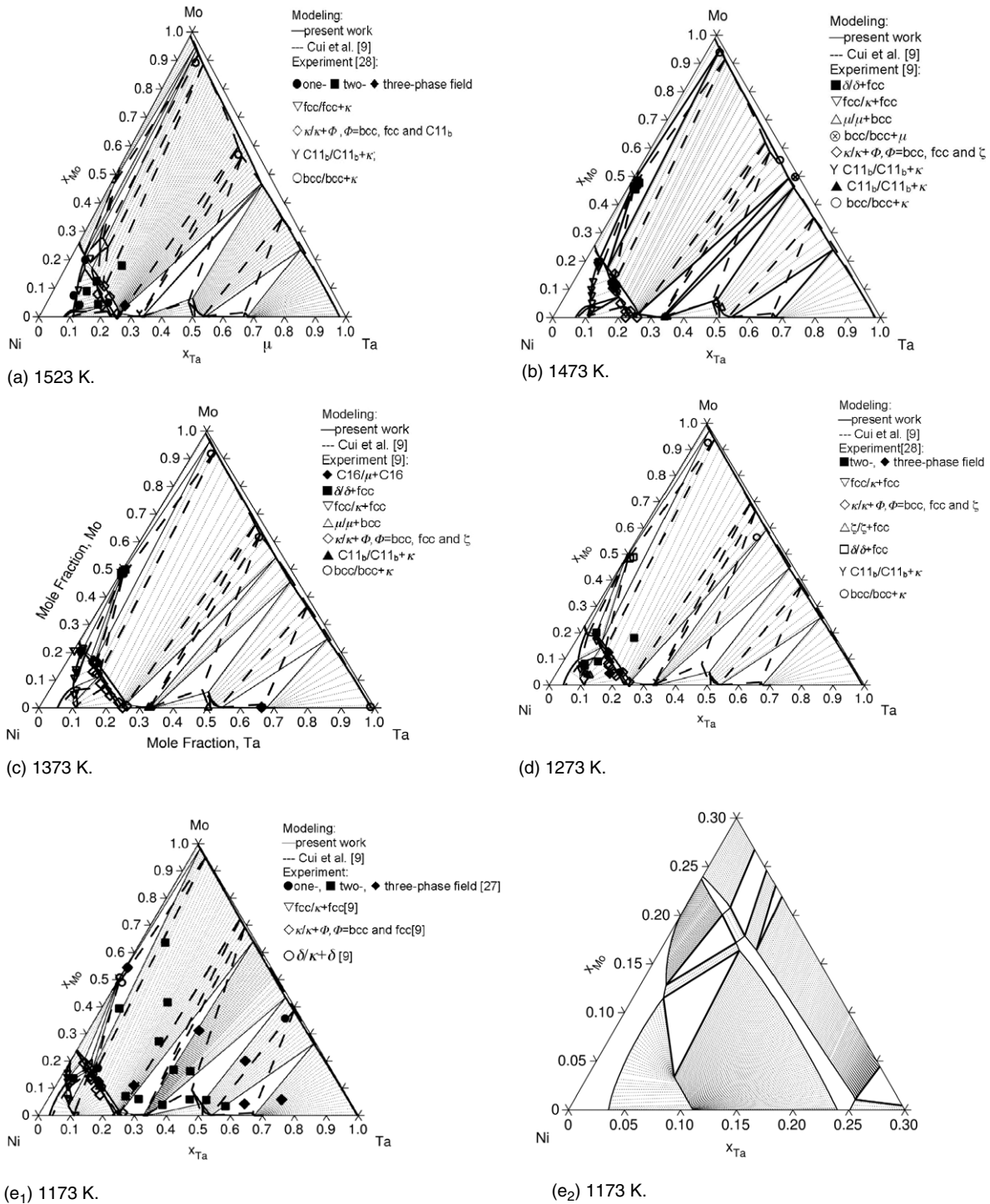
NiMo phase, the parameters  $\Delta G_{Ni:Ta:Mo}^{\delta}$ ,  $\Delta G_{Ni:Mo:Ta}^{\delta}$ ,  $\Delta G_{Ni:Ni:Ta}^{\delta}$  and  $\Delta G_{Ni:Ta:Ta}^{\delta}$  are evaluated with the first-principles data.

The bcc phase boundary data in the ternary Ni–Mo–Ta system by Cui et al. [9] and Chakravorty and West [28] are used to determine the ternary interaction parameters for the bcc phase. The interaction parameter  ${}^0L_{Ni:Mo,Ta}^{\zeta}$  for the ζ-Ni<sub>8</sub>(Mo, Ta) phase is evaluated with the experimental data for the ζ-Ni<sub>8</sub>(Mo, Ta)/ζ-Ni<sub>8</sub>(Mo, Ta)+fcc phase boundary [28]. The ternary parameters  $\Delta G_{Ta:Ta:Mo:Ni}^{\mu}$  and  ${}^0L_{Ta:Ta:Mo,Ta:Ni}^{\mu}$  for the μ phase are evaluated with the first-principles data in Table 6 and experimental data [9,27].

#### 4. Modeling results

The Ni–Ta phase diagram yielded by our modeling is shown in Fig. 1 together with previously proposed phase diagrams [6,7] and





**Fig. 5.** Isothermal sections of the Ni-Ta-Mo phase diagram, as computed from the present model for the indicated temperatures. Experimental data are also shown for comparison.

experimental data [6,7,10–16]. The invariant reactions calculated using the parameters in Tables 2, 4 and 5 are summarized in Table 7 and compared with the experimental data [10–13,15,16]. It is shown that the phase diagram in Fig. 1 produced by our model differs significantly from the previous reports [6,7], as highlighted in the following.

The major difference is that we assess the relative low temperature stability of the intermetallic compounds and sublattice end-member phases using first-principles calculations of the zero-Kelvin energies, as described above. Our result shows that the compounds C16-NiTa<sub>2</sub>, C11<sub>b</sub>-Ni<sub>2</sub>Ta, D0<sub>22</sub>-Ni<sub>3</sub>Ta, and ζ-Ni<sub>8</sub>Ta in the

Ni-Ta system are stable, while the compounds κ-Ni<sub>3</sub>Ta and μ-NiTa are not stable at 0 K. The model description of enthalpy of formation is plotted in Fig. 2 and compared with both experimental data and first-principles calculations. It is also shown that the modeling results of Cui and Jin [6] and Pan and Jin [7] are not consistent with the phase stabilities indicated by our first-principles calculations. The enthalpy of mixing for the liquid phase is shown in Fig. 3, and, again, our model provides a better agreement with the experimental data [19] than those reported by Cui and Jin [6] and Pan and Jin [7]. The calculated enthalpies of mixing for the bcc and fcc solutions are plotted in Fig. 4. In comparison with the first-

principles calculations, the model exhibits the appropriate general behavior, though the absolute agreement is rather poor. While this discrepancy, which may be attributed to the relaxation of the cell volume only, is distinct, the first-principles calculation for SQS is a useful option for quantifying the energetics of a solution phase at compositions where experimental measurements cannot be performed. Despite the limitations, in combination with other types of experimental data (e.g. phase boundaries), SQS calculations can contribute to the reliable assessment of thermodynamic model parameters.

The isothermal sections of the Ni–Mo–Ta system were calculated for temperatures 1523, 1473, 1373, 1273 and 1173 K, respectively, as shown in Fig. 5 along with the previously reported results [9] and the experimental data [9,27,28]. The results show that our modeling results differ significantly from the previous reports [9]. The calculated single  $\kappa$ -phase range shows significant difference between our result and that by Cui et al. [9] in Fig. 5, where our results are in good agreement with the experimental data [9,28]. In Fig. 5(a), the calculated isothermal section using the parameters by Cui et al. [9] shows the existence of the liquid phase on Ni-rich corner at 1523 K, while the experimental results by Chakravorty and West [28] did not show the liquid phase on Ni-rich corner. The other significant difference is shown in Fig. 5(e), where the stable  $\text{DO}_{10}$ - $\text{Ni}_3\text{Mo}$  and  $\kappa$ - $\text{Ni}_3\text{Ta}$  phases are treated as two different phases in this work, while Cui et al. [9] treat them as the same phase. Our treatment, thus, provides a basis for extending the model to other systems or subsystems with the  $\text{DO}_{10}$  ( $\text{Cu}_3\text{Ti}$  structure) and/or  $\kappa$  ( $\text{Pt}_3\text{Ta}$  structure) phases. In Fig. 5(e), our results show good agreement with the experimental data [9,27]. The third significant difference between our modeling and that of Ref. [9] is the direction of the tie-lines from the Ni-rich part towards Mo–Ta side of the system. This difference results from the Ni–Ta and Ni–Mo binaries, in which the first-principles results were employed in our modeling to determine the model parameters for both compound and solid solution phases. Fig. 2 and the figures in Ref. [8] show the calculated enthalpy of formation in which the difference between our model and that of Ref. [9] can be identified. Considering the experimental data for bcc/bcc +  $\kappa$  in Fig. 5(b) and (d), our results are reasonable, while those calculated bcc +  $\kappa$  two-phase field by Ref. [9] deviates from the experimental data [9,28]. To understand the stability of the fcc phase, we plotted the stable fcc phase field in the related composition triangle over a range of temperature in Fig. 6, which is useful for Ni-base superalloy design by showing the stable  $\gamma$ -fcc phase domain with related composition and temperature dimensions. To see the temperature dependent liquidus surface, we plot the liquidus projection for the Ni–Mo–Ta system along with the experimental data [28] in Fig. 7.

## 5. Summary and conclusions

By combining a CALPHAD approach and first-principles calculations, the Gibbs free energy functions of individual phases in the binary Ni–Ta and ternary Ni–Mo–Ta systems are evaluated, and the associated equilibrium phase diagrams are reported. The present work exhibits several key differences from previously reported thermodynamic modeling, which are that (i) the first-principles calculated enthalpies of formation indicate that the compound  $\text{DO}_{22}$ - $\text{Ni}_3\text{Ta}$  is stable while  $\kappa$ - $\text{Ni}_3\text{Ta}$  and  $\mu$ -NiTa are metastable at 0 K, (ii) the phase boundaries in the binary Ni–Ta system are in better agreement with experimental observations, (iii) the calculated phase diagrams for the Ni–Mo–Ta system show good agreement with the experimental data.

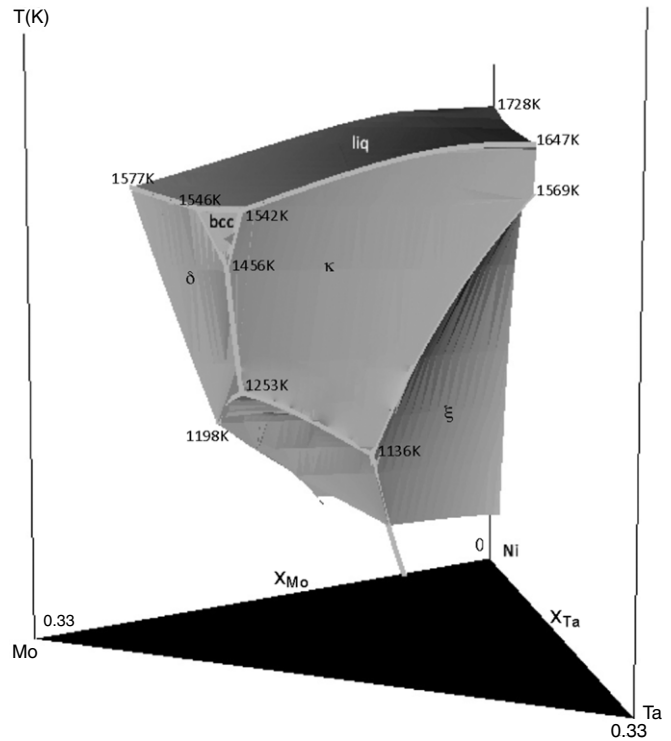


Fig. 6. The fcc single-phase field, as computed using the present model.

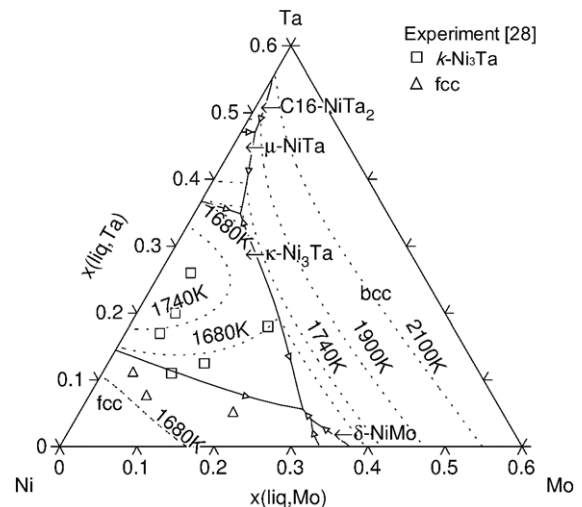


Fig. 7. The liquidus composition-plane projection indicating the primary phases and comparing with experimental data [28] for the Ni–Mo–Ta system, as computed using the current model.

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## Appendix. Supplementary data

Supplementary data associated with this article can be found, in the online version, at doi:10.1016/j.calphad.2009.06.006.

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